

Start-to-end commissioning simulation for the HALF storage ring*

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Hefei advanced light facility (HALF) is a 4th-generation diffraction-limited light source which started construction in 2023. The storage ring has an energy of 2.2 GeV and an extremely low emittance of less than $100 \text{ pm} \cdot \text{rad}$. It contains 20 superperiods of the modified hybrid 6-bend achromat with a circumference of about 480 m. In reality, the real storage ring is different from the ideal lattice due to various kinds of errors. Those errors come from many sources, e.g., misalignment of components, imperfect magnetic fields, RF cavities, etc. Due to the small dynamic aperture and strong nonlinear effects, the errors have a serious effect on the 4th-generation storage ring, which brings great difficulties to its commissioning. To figure out the practical performance of the lattice with those errors, a start-to-end commission simulation is performed in this study, which also helps to verify the effectiveness of the commissioning of the HALF storage ring. In addition, the commissioning simulation process provides the basis for the development of the commissioning software for the HALF storage ring. Details and results of the commissioning simulation are reported in the paper.

Keywords: HALF, Storage ring, Commissioning simulation, Beam-based alignment, LOCO.

I. INTRODUCTION

The synchrotron radiation source has many properties such as high intensity, high brightness, transverse coherence, good time structure, very broad and continuous spectral range, etc [1, 2]. Since the 1970s, dedicated synchrotron radiation light sources have been developed as one of the most powerful scientific research tools over decades [3, 4]. The 4th-generation synchrotron radiation light source is proposed in recent years [5, 6]. By reducing the emittance of the electron beam in the storage ring, the brightness and coherence of the diffraction-limited synchrotron radiation are increased by two to three orders of magnitude compared with the 3rd-generation light sources [7, 8]. This huge and qualitative leap will greatly enhance the research capacity of synchrotron radiation, making it better to apply to the basic and applied researches. At present, there are several 4th-generation synchrotron radiation light sources that are already built, under construction, built or planned for upgrade in the world [9–13].

The Hefei advanced light facility (HALF) is a 4th-generation light source, which is under construction in Hefei, China [14]. The HALF storage ring contains 20 superperiods with modified hybrid 6-bend achromat with an emittance of less than $100 \text{ pm} \cdot \text{rad}$. The goal of the HALF project is to build a high-performance synchrotron radiation light source in the VUV to soft X-ray region.

In a 4th-generation light source storage ring, the quadrupoles with strong strengths are used in order to obtain a low emittance, which results in the large negative chromaticities. To correct the chromaticities, intense sextupoles are adopted, leading to strong nonlinearity. Because of the strong quadrupoles and sextupoles, the magnetic field feed-down effects of the off-axis beam are large. Therefore, the errors of the machine components can severely affect the linear

optics and dynamic performance of the storage ring. Besides, the dynamic aperture of the ultra-low emittance storage ring is much smaller than that of the 3rd-generation ring, which causes additional difficulties to its commissioning. In order to figure out the performance of the storage ring and verify the effectiveness of the correction to various errors, a start-to-end simulated commissioning is essential. The simulated correction process is also the basis for the online commissioning of the HALF storage ring in the future. A recently developed Commissioning Simulation toolkit (SC) [15–19] based on the commonly used Accelerator Toolbox (AT) [20, 21] is adopted in this study.

The subsequent sections of this paper are organized as follows. In Sect. II, the basic performance and layout of the HALF storage ring are introduced. In Sect. III, settings of various errors are given. The performance of the storage ring without any correction is shown in Sect. IV. In Sect. V, the correction chain of the simulated commissioning process is shown. Finally, the summary and conclusion are given in Sect. VI.

II. THE HALF STORAGE RING

A. Lattice

The modified hybrid 6-bend achromat lattice structure is adopted by the HALF storage ring in order to obtain an ultra-low emittance [22, 23]. The natural emittance is $85.8 \text{ pm} \cdot \text{rad}$ with an energy of 2.2 GeV. The ring is composed of 20 identical cells which provides 20 long and 20 short straight sections. The optic functions and layout of the lattice is shown in Fig. 1. The unit cell contains 6 dipoles, 4 reverse bends, 16 quadrupoles, 8 sextupoles and 2 octupoles. All dipole magnets are longitudinal gradient bending (LGB) magnets which help to reduce the nature emittance along with the reverse bends. The quadrupoles are powered independently in order to tune the optic functions. The sextupoles are used to correct the chromaticities and optimize the dynamic performance. To save space, the slow orbit correctors

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and skew quadrupole components are combined to those sextupoles. The main parameters of the HALF storage ring are shown in Table 1.

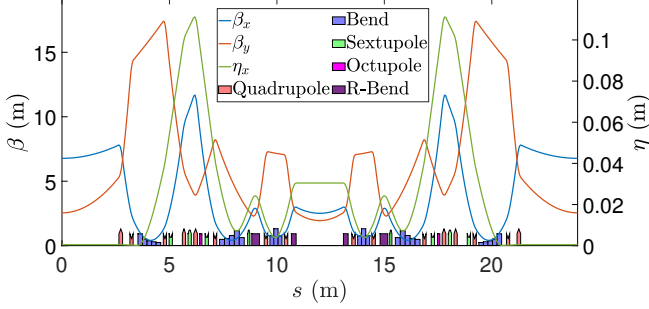


Fig. 1. (Color online) Optic functions of the HALF storage ring in one unit cell.

Table 1. Main parameters of the HALF storage ring.

Parameter	Value	Unit
Energy	2.2	GeV
Circumference	479.86	m
RF frequency	499.8	MHz
Harmonic number	800	-
Natural emittance	85.8	pm · rad
Transverse tunes	48.19/17.19	-
Natural Chromaticities	-81.6/-56.6	-
Corrected Chromaticities	+3/+3	-
Momentum compaction factor	9.4×10^{-5}	-
Damping partition number	1.36/1.00/1.64	-
Damping time	28.5/38.8/23.7	ms
Bunch length	1.32	mm
Natural energy spread	0.61×10^{-3}	-
Energy loss per turn	181.4	KeV
Synchrotron frequency	2.06	kHz
Linear energy acceptance	8.14	%

B. Dynamic performance

The HALF storage ring is carefully designed to optimize its dynamic performance. The on-momentum 4D and 6D dynamic apertures (DA) of the HALF storage ring are shown in Fig. 2, which are about 13 mm and 8 mm in the horizontal plane respectively. Benefiting from the relatively large DA, the off-axis injection scheme can be adopted, while it still causes difficulties to the ring commissioning. The local momentum aperture (LMA) is shown in Fig. 3, which is obtained by 6D tracking.

C. Monitors and correctors configuration

The configuration of the correctors and the beam position monitors (BPMs) is shown in Fig. 4. Each cell contains 12 horizontal and vertical orbit correctors and 12 BPMs. Among

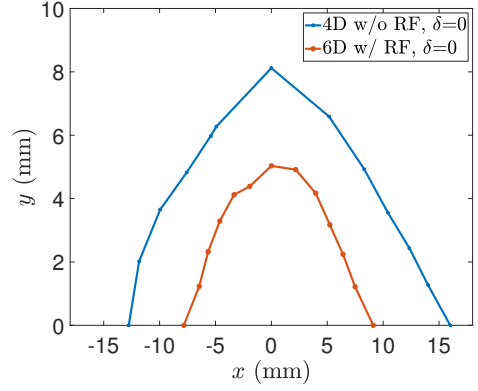


Fig. 2. (Color online) On-momentum dynamic aperture of the HALF storage ring.

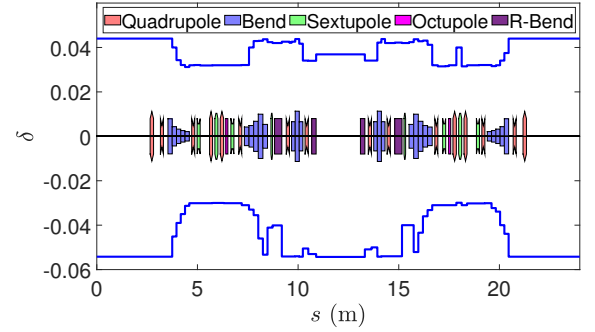


Fig. 3. (Color online) Local momentum aperture of the HALF storage ring.

those correctors, 8 are combined to the multi-function sextupoles, and 4 isolated correctors are located at the ends of the straight sections. Skew quadrupole coils are combined to the sextupole families SD1, SD2 and SF1 in order to correct the coupling induced by the misalignment of the magnets. Since the main vacuum chamber is a circular one with a diameter of 26 mm, a physical aperture with a radius of 13 mm is set to all elements.

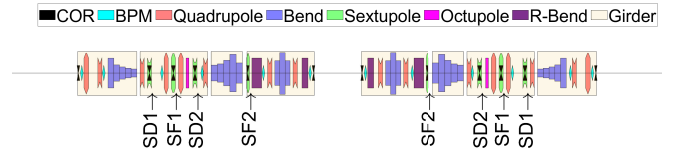


Fig. 4. (Color online) The configuration of correctors and BPMs in one unit cell.

III. ERROR SETTINGS

Before the commissioning simulation process, we need to incorporate various types of errors into the lattice to imitate the real machine. The random errors are generated based on

a 2σ -truncated Gaussian distribution, where σ represents the root mean square (RMS) of the errors.

A. Misalignment and magnetic field errors

The misalignment and field errors of the main magnets are detailed in Table 2. In a real machine, magnets are installed on the girders. The magnets have misalignment errors while the girders also have misalignment errors. Therefore, the overall misalignment of the magnets are the sum of their own errors combined with the girder errors. The fields of the bends and quadrupoles are set with a 5×10^{-4} RMS fractional error. And the field errors of other multipoles are set to 1×10^{-3} .

B. BPMs and correctors

The resolution of the BPM turn by turn (TBT) data is set to $1 \mu\text{m}$, and the resolution for the closed orbit slow acquisition (SA) data is set to $0.1 \mu\text{m}$. A calibration error of the sum signal of 3% is assumed. The maximum strength of the orbit correctors is 1 mrad in both horizontal and vertical planes. To correct the ring coupling, skew quadrupoles with a maximum strength of 0.27 m^{-2} are adopted. The parameters of the BPMs and correctors are shown in Table 3.

C. RF errors

The errors of the RF system include the frequency, voltage and phase errors, which majorly comes from calibration, system shifting, closed orbit error and beam energy error of the storage ring, etc. The error information of the RF cavity can be obtained with beam transmission. The initial phase error of the RF cavity is usually large. The errors of the RF system are presented in Table 4.

D. Injection errors

As a 4th-generation light source, the HALF storage ring has a relatively large dynamic aperture, which greatly improves the ring acceptance and offers the possibility of using the off-axis injection scheme. The injection system of the HALF storage ring adopts the pulsed nonlinear kicker (NLK) method [24, 25], which is simple in structure and has little disturbance to the stored beam. By using the pulsed NLK, the injected bunch is directly kicked into the phase space within the acceptance of the storage ring. The injected beam is then damped onto the closed orbit of the stored beam after several damping times. The stored beam, which goes through the central field-free region, has a little impact from the NLK, making the injection transparency for the light source users.

A full-energy linac with an energy of 2.2 GeV is used as the injector of the storage ring. The injected beam from the linac has an emittance of $500 \text{ pm} \cdot \text{rad}$. The NLK along with

a septum is located in one straight section, forming the whole injection system. The parameters of the injected beam at the injection position are shown in Tables 5, and the errors are described in Table 6.

IV. PERFORMANCE BEFORE CORRECTION

To figure out the difference between the ideal lattice and the actual one with errors, the performance of the HALF storage ring is studied before any correction. In a 4th-generation light source, the closed orbit (CO) may be absent without correction. The existence of the CO is investigated by scaling the global error factor as depicted in Fig. 5. It shows that the CO exists when the scaling factor is less than 20%. As the factor increases to 100%, the existence possibility of the CO decreases to less than 20%. The deviation of the CO as a function of the global error factor is shown in Fig. 6. We can see that as the global error factor increases, the deviation increases until the closed orbit is lost. When the factor increases to a certain level, the orbit deviation reaches its maximum before the beam is lost.

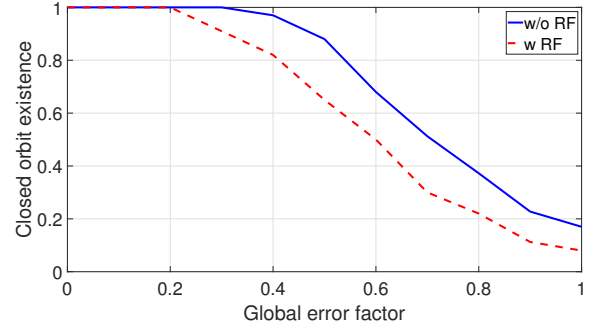


Fig. 5. (Color online) The closed orbit existence before any correction. The closed orbit exists when the scaling factor is less than 20%. As the factor increases to 100%, the existence possibility of the CO decreases to less than 20%.

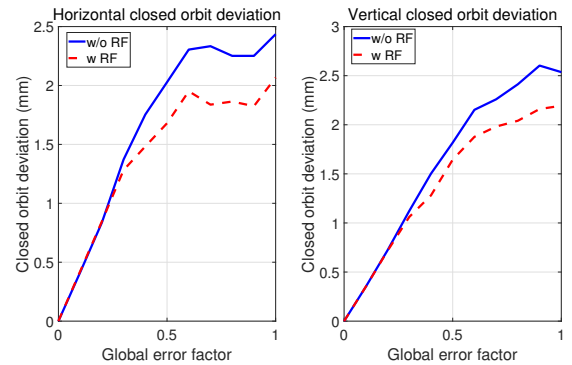


Fig. 6. (Color online) Deviation of the closed orbit as a function of the error scaling factor.

Table 2. Misalignment errors and field errors for the main magnets and girders. dx, dy, and ds represent the shift errors in the horizontal, vertical, and longitudinal plane respectively. rx, ry, and rs denote the rotation errors around the horizontal, vertical, and longitudinal axis respectively.

Element	dx(μm)	dy(μm)	ds(μm)	rx(μrad)	ry(μrad)	rs(μrad)	Field
Bends	200	200	150	200	200	100	5×10^{-4}
Quadrupoles	30	30	150	100	100	100	5×10^{-4}
Sextupoles	30	30	150	100	100	100	1×10^{-3}
Octupoles	30	30	150	100	100	100	1×10^{-3}
Girder	100	100	200	100	100	100	-

Table 3. Errors of the BPMs and corrector magnets.

Parameter	Value	Unit
BPM noise for TBT	1	μm
BPM noise for CO	0.1	μm
BPM calibration error	3	%
BPM offset	200	μm
BPM roll around s -axis	100	μrad
BPM gain	5	%
CM calibration error	5	%
CM strength limit	1	mrad
CM offset	200	μm
CM roll	200	μrad
Skew quadrupole strength limit	0.27	m^{-2}
Skew quadrupole calibration error	5×10^{-4}	-

Table 4. RF cavity errors.

Parameters	Values	Units
Voltage offset	1	%
Frequency offset	1×10^3	Hz
Time lag offset	90	Deg

Table 5. Parameters of the injected beam.

Parameters	Values	Units
ϵ_x/ϵ_y	500/500	$\text{pm} \cdot \text{rad}$
σ_x	58.18	μm
$\sigma_{x'}$	8.59	μrad
σ_y	35.70	μm
$\sigma_{y'}$	14.01	μrad
σ_δ	0.05	%
σ_ϕ	15	ps

Table 6. Errors of the injected beam.

Parameters	Systematic	Jitter	Units
Δx	100	10	μm
$\Delta x'$	100	10	μrad
Δy	100	1	μm
$\Delta y'$	100	1	μrad
$\Delta E/E$	5×10^{-4}	1×10^{-4}	-
$\Delta\phi$	0	0.1	Deg

V. SIMULATED COMMISSIONING FOR THE HALF STORAGE RING

In this section, the correction chain of the simulated commissioning for the HALF storage ring is presented, which includes: A) Initial transmission correction (the first-turn trajectory correction and second-turn trajectory correction), B) Trajectory beam-based alignment, C) Injection correction, D) Sextupole ramping, E) RF correction, F) Beam-based alignment and G) Optics correction. In order to avoid the influence of the sextupoles and RF system on the beam dynamics, we turn them off at the beginning of commissioning.

A. Initial transmission

The beam usually fails to form a closed orbit and even can not pass through a complete turn in many cases at the beginning of the ring commissioning. To obtain the first-turn beam, the trajectory response matrix of the ideal lattice is used to perform trajectory correction at the BPMs which have turn-by-turn beam position signals. The correction process is repeated to let more BPMs have position signals. If the iteration yields no effect, the injected beam is scanned and the kick strengths of the correctors before the failure position are tuned until the beam passes through this BPM [26]. After the first-turn trajectory correction, the particles are expected to travel tens of turns. To further improve transmission of the beam, the trajectory of the second turn is corrected to be close to the first one. After the second-turn trajectory correction, more turns are expected to be achieved by the injected particles. The cumulative distribution functions (CDFs) of the beam loss under the first-turn and second-turn trajectory corrections are shown in Fig. 7.

B. Trajectory beam-based alignment

Due to the magnetic field feed-down effect, the electron beam would receive a kick when it travels away from the center of the quadrupoles. This additional kick has a significant impact on the beam transmission, especially for the low-emittance storage rings adopting the quadrupoles with strong strengths. To avoid this effect, the beam should pass through the centers of all quadrupoles. The beam-based alignment (BBA) technique is used to determine the center of a

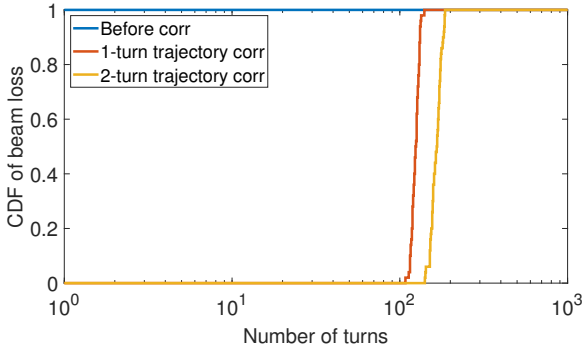


Fig. 7. (Color online) The cumulative distribution function of the beam loss after the first-turn and second-turn trajectory corrections.

quadrupole by using a nearby BPM and the orbit correctors. The beam position $\mathbf{X}(s_0)$ (trajectory or orbit) of the particles at the quadrupole position s_0 can be described by

$$\mathbf{X}(s_0) = x_0 \hat{x} + y_0 \hat{y}, \quad (1)$$

where x_0 and y_0 are particle offsets relative to the quadrupole magnet center in the horizontal and vertical plane respectively.

Due to the feed-down effect, this quadrupole can generate a dipole field,

$$B_x = B_0 \rho_0 K y_0, \quad (2)$$

$$B_y = B_0 \rho_0 K x_0, \quad (3)$$

where $B_0 \rho_0$ is the magnetic rigidity, K is the normalized quadrupole strength.

By changing the quadrupole strength with ΔK , the variation of the dipole field is given by

$$\Delta B_x = B_0 \rho_0 \Delta K y_0, \quad (4)$$

$$\Delta B_y = B_0 \rho_0 \Delta K x_0. \quad (5)$$

For the closed orbit scenario, this variation results in an orbit change at location s [27],

$$\Delta \mathbf{X}(s) = \Delta K \mathcal{T}(s, s_0) \mathbf{X}(s_0), \quad (6)$$

$$\mathcal{T}(s, s_0) = \left(\frac{1}{1 - K_0 \frac{L_0 \beta(s_0)}{2 \tan(\pi \nu)}} \right) \times \frac{\sqrt{\beta(s) \beta(s_0)}}{2 \sin(\pi \nu)} \cos(|\phi(s) - \phi(s_0)| - \pi \nu), \quad (7)$$

where L_0 is the length of the quadrupole, $\beta(s_0)$ and $\beta(s)$ are the beta functions at the location of the quadrupole and the observation point respectively. $\phi(s_0)$ and $\phi(s)$ are the betatron phases, and ν is the betatron tune.

The function $\mathcal{T}(s, s_0)$ is related with the Courant-Snyder (C-S) parameters, which can be considered as a constant

when the change of quadrupole strength ΔK is small. Then, the orbit change $\Delta \mathbf{X}(s)$ would be proportional to the orbit offset $\mathbf{X}(s)$. If the beam goes through the center of the quadrupole, the orbit change should theoretically be equal to zero. Using this principle, the quadrupole center can be obtained through measuring the orbit changes by varying the beam position in this quadrupole with a change in its strength ΔK [28]. If the beam orbit is least affected by changing the strength of the target quadrupole, the nearest BPM reading is considered as the center of the quadrupole.

The BBA process can also be applied to the trajectory case. The difference is that for the trajectory BBA, the beam position change is generated by adjusting the initial condition of the injected beam. After the trajectory BBA, the CDF of the beam loss is shown in Fig. 8, where an improvement in the beam transmission is seen.

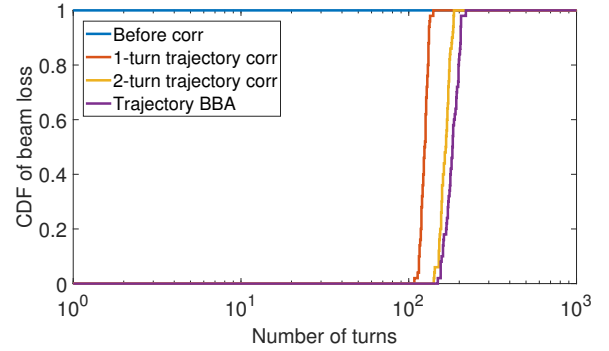


Fig. 8. (Color online) The cumulative distribution function of the beam loss after trajectory BBA.

C. Injection correction

To correct the static injection error, the injection correction is needed to obtain a better choice of the injection position. In Fig. 9, the 1st-turn BPM readings in the upstream and 2nd-turn BPM readings in the downstream of injection position are (x_u, y_u) and (x_d, y_d) , where $x_{u,d}$ and $y_{u,d}$ are the BPM reading in the horizontal and vertical planes respectively. And the distances between the BPM and injection position are l_u and l_d . Then the injection point can be moved the position,

$$x_{\text{inj}} = l_d \frac{x_u - x_d}{l_u + l_d} + x_d, \quad (8)$$

$$y_{\text{inj}} = l_d \frac{y_u - y_d}{l_u + l_d} + y_d, \quad (9)$$

and the injection angle is given by

$$x'_{\text{inj}} = \frac{x_d - x_u}{l_u + l_d}, \quad (10)$$

$$y'_{\text{inj}} = \frac{y_d - y_u}{l_u + l_d}. \quad (11)$$

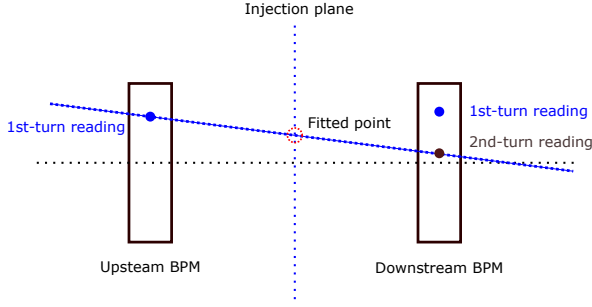


Fig. 9. (Color online) A schematic of the injection correction.

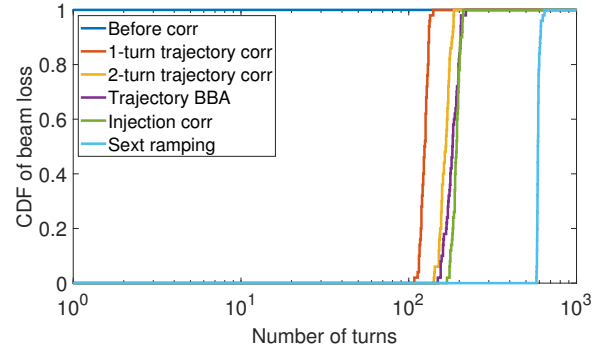


Fig. 11. (Color online) The cumulative distribution function of the beam loss after the sextupoles ramping.

266 The CDF of the beam loss after the injection correction is
267 shown in Fig. 10.

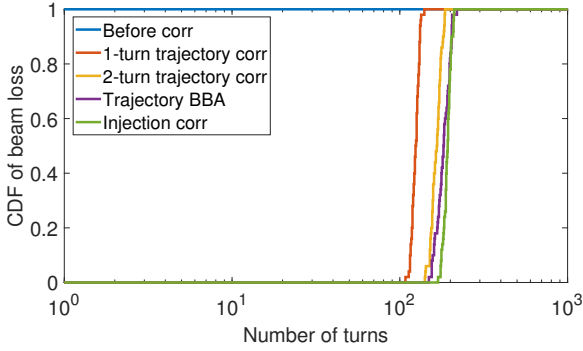


Fig. 10. (Color online) The cumulative distribution function of the beam loss after the injection correction.

D. Sextupole ramping

269 Due to the large nonlinear effect induced by the sextupoles,
270 we turn them off at the beginning of the commissioning. For
271 a storage ring, the chromatic sextupoles are needed to cor-
272 rect the chromaticities to positive values in order to avoid the
273 head-tail instability. Also the harmonic sextupoles are com-
274 monly adopted to optimize the dynamic performance of the
275 storage ring. For sextupole ramping, the strengths of all sex-
276 tupoles are increased in 5 steps. After each step, the trajec-
277 tory is corrected to the reference trajectory obtained from the tra-
278 jectory BBA. If necessary, the tune scan can be performed by
279 using two quadrupole families to improve the beam transmis-
280 sion. Until now the synchrotron radiation of all magnets are
281 on while the RF is turned off. The radiation loss per turn for a
282 single particle is 181.4 keV. The linear energy acceptance of
283 the HALF storage ring is 8.1%. This means the particles can
284 travel about 987 turns ideally. In Fig. 11, we can see that the
285 particles can go through near 600 turns, which shows an ef-
286 fective trajectory correction. Next we turn the RF on to form
287 the closed orbit.

E. RF correction

289 The BPM turn-by-turn (TBT) data can be used to correct
290 the phase and frequency errors of the RF system. Due to the
291 horizontal dispersion, the change of the horizontal beam po-
292 sition Δx induced by the energy variation ΔE is described
293 as [29]

$$\frac{\Delta x}{\eta_x} = \frac{\Delta E}{E}, \quad (12)$$

295 where η_x is the horizontal dispersion, and E is the beam en-
296 ergy. The beam energy variation with the turn number n can
297 be expressed as [30, 31]:

$$\Delta E_n = eV \sin(\Delta\omega T_0 n + \varphi_0 + \Delta\varphi) - U_0, \quad (13)$$

299 where V is the rf voltage, φ_0 is the synchronous phase, T_0 is
300 the synchronous period, U_0 is the radiation energy, $\Delta\omega$ and
301 $\Delta\varphi$ are the frequency and phase errors.

302 By integrating Eq. 13 over the turn number n and combin-
303 ing with Eq. 12, the beam energy change after n turns is given
304 by

$$\frac{\Delta x}{\eta_x} = \frac{E_n - E_0}{E} = -\frac{eV}{\Delta\omega T_0 E} [\cos(\Delta\omega T_0 n + \varphi_0 + \Delta\varphi) - \cos(\varphi_0 + \Delta\varphi)] - \frac{U_0 n}{E}. \quad (14)$$

306 Eq. 14 shows that the orbit variation is a function of the
307 frequency error $\Delta\omega$ and phase error $\Delta\phi$. To correct the fre-
308 quency and phase errors, we can adjust $\Delta\omega$ and $\Delta\phi$ to let Δx
309 be 0. To simplify this procedure, we can do this correction
310 separately.

311 For a real machine, the frequency error is usually small. To
312 correct the phase error firstly, we assume $\Delta\omega$ to be 0. Then
313 Eq. 14 turns out to be

$$\frac{\langle \Delta x \rangle}{\eta_x} = \frac{\Delta x}{n\eta_x} \approx \frac{eV}{E} \sin(\varphi_0 + \Delta\varphi) - \frac{U_0}{E}, \quad (15)$$

315 which shows that the average horizontal beam position vari-
316 ation $\langle \Delta x \rangle$ is a sine function of the rf phase φ_0 . After three

iterations of the phase correction, the zero crossing is finally determined as the synchronous phase as shown in Fig. 12. To ensure at least 100 turns of beam transmission for the subsequent frequency correction, the tune scan is performed by changing the strengths of two quadrupole families after the first phase correction.

To correct the phase error $\Delta\phi$, $\Delta\omega T_0$ can be treated as a small quantity. Then Eq. 14 can be written as

$$\frac{\langle\Delta x\rangle}{\eta_x} = \frac{\Delta x}{n\eta_x} \approx \frac{eV}{E} \left[\frac{1}{2} \Delta\omega T_0 n \cos(\varphi_0 + \Delta\varphi) + \sin(\varphi_0 + \Delta\varphi) \right] - \frac{U_0}{E}, \quad (16)$$

where the average beam position variation $\langle\Delta x\rangle$ is a linear function of the frequency error $\Delta\omega$. A line is fitted and the zero crossing is considered as the synchronous frequency after three iterations as shown in Fig. 13.

In the RF correction, the synchrotron motion should be taken into consideration. The number of the evaluated turns should be significantly smaller than 304 turns for the HALF storage ring, which is related to the synchrotron frequency of 2.06 kHz. Therefore, the average position of 20 turns are adopted. The CDF of the beam loss is shown in Fig. 14. The beam can pass through more than 1000 turns and finally becomes a stored beam.

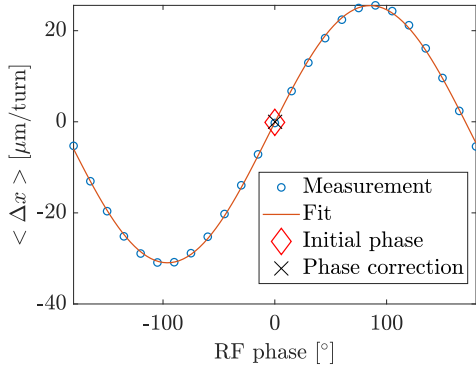


Fig. 12. (Color online) RF phase correction result in the final iteration.

F. Beam-based alignment

In this step, the closed orbit BBA is performed in order to obtain the golden orbit. The method used in the CO BBA is identical to the one mentioned in the previous subsection VB, except in the way of measuring the closed orbit. In the CO BBA, we use the orbit correctors to generate different kick strengths on the beam to move the beam inside the target quadrupoles. After performing the CO BBA, the closed orbit is corrected to the reference orbit. After the orbit correction, the strengths of all correctors with 10 sets of random error seeds are shown in Fig. 15. To mitigate the magnet feed-down

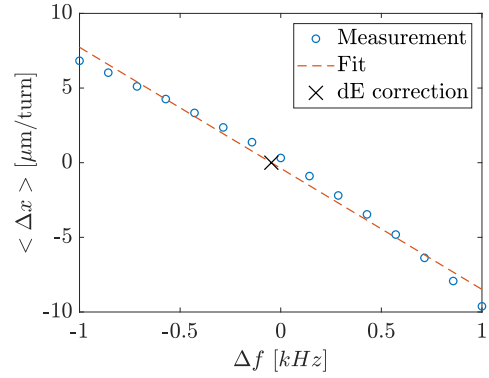


Fig. 13. (Color online) RF frequency correction result in the final iteration.

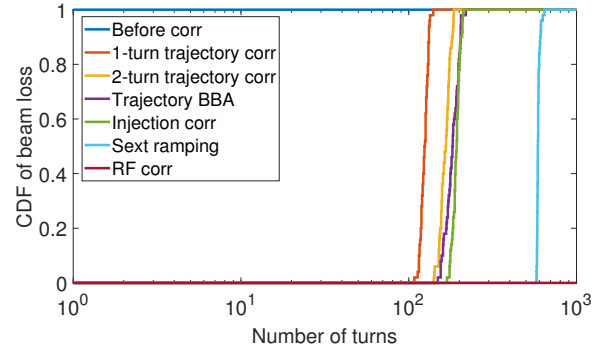


Fig. 14. (Color online) The cumulative distribution function of the beam loss after performing RF correction. The beam can be store for more than 1000 turns.

effect, moving the beam to the quadrupole centers is critical for the optics correction.

G. Optics correction

The linear optics is essential for the storage ring, which mainly includes the beta and dispersion functions. Due to the lattice errors, the optics would deviate from their ideal values, which can result in the shifts of the betatron tunes, reduction of the dynamic aperture, etc. To correct the linear optics, a commonly used technique called the LOCO (Linear Optics from Closed Orbit) is performed, which can restore the periodicity of the storage ring, decrease the negative effects of nonlinear resonances, and increase the beam lifetime and DA [32, 33]. All quadrupoles are used for optics correction since they are powered independently. To correct the coupling, the skew quadrupole combined to the sextupole families SD1, SD2 and SF1 are used. The correction results for one error set are shown in Fig. 16 and Fig. 17. One can see that the beta beating and dispersion deviation is greatly reduced to a low level. The periodicity of the lattice is restored as shown in Fig. 18. The betatron tunes are (0.193, 0.195), which are close to the ideal values (0.190, 0.190).

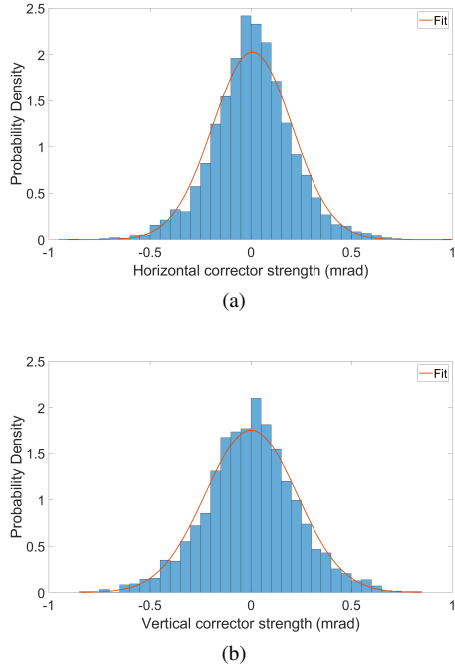


Fig. 15. Distribution of the corrector strengths after correcting the beam to the golden orbit: (a) Horizontal, (b) Vertical. The standard deviation of horizontal corrector strengths is 0.20 mrad, and the standard deviation of vertical corrector strengths is 0.23 mrad.

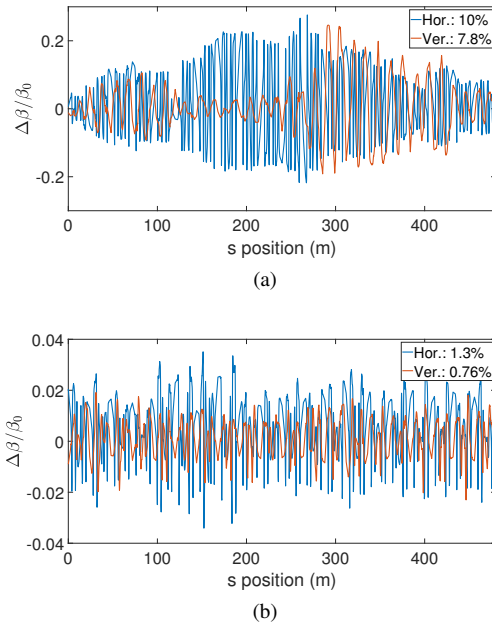


Fig. 16. Beta beating of the HALF storage ring before and after optics correction: (a) Before correction, (b) After correction. The horizontal beta beating (RMS) is reduced from 10% to 1.3% while the vertical beta beating is reduced from 7.8% to 0.76%.

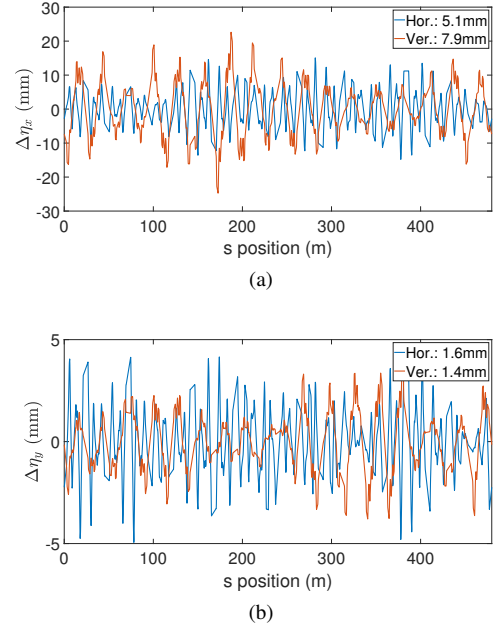


Fig. 17. Dispersion deviation of the HALF storage ring before and after optics correction: (a) Before correction, (b) After correction. The horizontal dispersion deviation (RMS) is reduced from 5.1 mm to 1.6 mm while the vertical dispersion deviation is reduced from 7.9 mm to 1.4 mm.

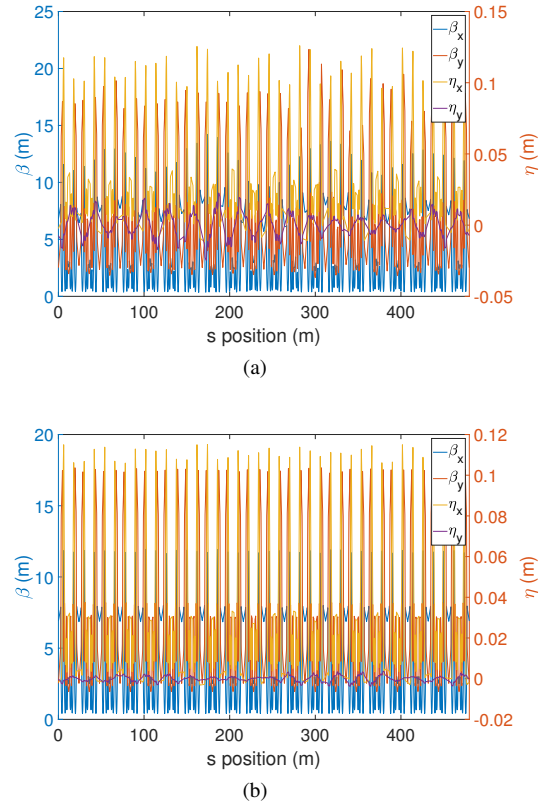


Fig. 18. Linear optics of the HALF storage ring before and after correction: (a) Before correction, (b) After correction. It is obvious that the periodicity of the lattice is restored.

VI. SUMMARY AND CONCLUSION

ulated commissioning.

The start-to-end commissioning simulation for the HALF storage ring is performed. For this 4th-generation light source ring, the electron beam can not form the closed orbit with errors at the beginning of the commissioning. After a series of effective correction procedures, the beam is stored, and the optic functions of the lattice are corrected to the ideal model. To figure out the recovery of the dynamic performance of the storage ring, the start-to-end commissioning simulation is performed with 10 sets of random error seeds. After the correction, the 6D dynamic aperture of the ring is close to the ideal one, as is seen in Fig. 19. It shows that the whole correction chain presented above is effective and successful. It guarantees a significant increase of our confidence in commissioning the real machine in the future. Also the commissioning software is going to be developed based on this sim-

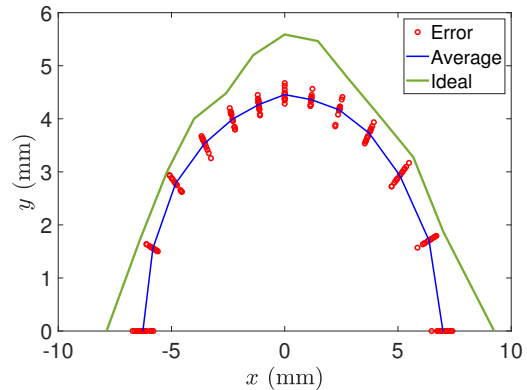


Fig. 19. (Color online) On-momentum 6D dynamic aperture of the HALF storage ring after correction.

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